Journal of Manufacturing Engineering, September 2015, Vol. 10, Issue. 3, pp 130-135



EFFECT OF SIC AND AL2O3 REINFORCED PARTICULATES ON FRICTION STIR WELDED JOINT OF MAGNESIUM ALLOY AZ91

^{*} Md.Aleem Pasha¹, Ravinder Reddy P², Laxminarayana P³ and Shtiaq Ahmad Khan⁴

¹Osmania University, Hyderbad, India. ²Mechanical Engineering Department, CBIT, Hyderabad, India. ³Mechanical Engineering Department, Osmania University, Hyderabad, India. ⁴Automotive Industry, Pune, India.

ABSTRACT

This work was focused on to study the changes in behavior of Magnesium alloy friction stir welded joint by inserted additional 'SiC' and 'Al₂O₃' Reinforced particles with an appropriate volume fraction at weld interface by providing gap provision and interlocking between two metal plates to form a metal matrix composite at weld interface which were enhanced the mechanical properties. Used a friction stir welding apparatus to stir reinforced particles into two base materials and a friction stir weld was formed. Moreover, metallurgical bonding was achieved between the reinforced particles and the base materials. Quality assessment included the visual inspection, temperature measurement in welding region, Tensile strength testing, impact strength testing, and hardness measurements. Research aimed at the recognition of FSW abilities to weld Magnesium alloys by inserting reinforced particles at weld interface and influence of reinforced particles and interlocking on weld properties. The research results have revealed that magnesium alloy AZ91 were weldable with reinforced particles at weld interface increasing the mechanical properties such as hardness, yield strength, and small reduction in ultimate strength than base metal. But at the same time elongation decreases and the behavior of Material changes from ductile to brittle.

Keywords: Magnesium Alloy AZ91, Reinforced Particles Sic, Al2O3, Interlocking and Mechanical Properties.

1. Introduction

Magnesium has the density as small as 1.7 g/cm³, which is the lowest among all the structural metals or alloys [1]. Such an outstanding property makes it extremely important for manufacturing light weight structures. However, magnesium is very soft. It is necessary to add either alloy elements or reinforcements to make it stronger. Recently, friction stir processing particle reinforced magnesium has been studied [2, 3, 4, 5–8]. In the work performed by Lee et al. [8], Nano scale SiO₂ with the dimension of 20 nm was added into an AZ61 magnesium alloy.

Magnesium alloys are unique structural materials having high specific strength and capability to absorb shock and vibration energy [9]. cast Mg alloy AZ91D containing 9 % Al(mass) and 1 %Zn (mass) has been most widely used in engine building industries and aircraft due to its low density, high castability and good mechanical properties.

However, the main drawback of Mg alloy as a structural material is its high chemical activity leading

in many cases to a low welding characteristics and corrosion resistance. This means that in the conventional fusion welding process there should be such a treatment procedure before or after welding of Mg alloys.

This new technique has resulted in low distortion and high joint strength compared to other techniques. Moreover FSW is capable of joining all kinds of Al alloys. But very little is known about the weldability of Mg alloys [13, 14] since recent studies have nearly restricted to that of Al alloys.

There have to be more knowledge about the weldability of Mg alloys. The objectives of this work are to develop an understanding of the micro structural development of friction stir welds on an AZ91Mg alloy, and to determine the weldability of magnesium alloys by adding reinforced particulates at weld interface, effect of reinforced particles on the mechanical properties of FSW of Magnesium alloy AZ91.

*Corresponding Author - E- mail: aleemphd2013@gmail.com

www.smenec.org

© SME





Fig.1 Friction Stir Welding Process

Frictions stir welding is a solid-state joining technique, The main principle of FSW involves inserting a non-consumable rotating tool with a specially designed pin and shoulder into the butting edges of plates or sheets to be joined and traversed along the line of joint (Fig. 1). The tool provides two primary functions i.e heating of work piece, and movement of material to produce the joint. The heating is accomplished by friction between the tool and the work piece and plastic deformation of work piece. The localized heating softens the material around the pin and combination of tool rotation and translation leads to movement of material from the front of the pin to the back of the pin. As a result of this process a joint is produced in 'solid state' [9-10]. Because of various geometrical features of the tool, the material movement around the pin can be quite complex [11]. During FSW process, the material undergoes intense plastic deformation at elevated temperature, resulting in generation of fine and equiaxed recrystallized grains [12-15].

The metal-coated reinforcement particles with an appropriate volume fraction are inserted into the gap between two metal plates or two metal matrix composite (MMC) plates.The reinforcement particles are stirred into the metal plates or the MMC plates by friction stir welding (FSW) to form a butt weld metal containing reinforcement particles. Or the metal-coated reinforcement particles deposited on the surface of the metal plates or the MMC plates and then are stirred into base material of the metal plates. The metal-coated reinforcement particles are uniformly distributed in a weld metal by such stirring, the coated metal layer on the surface of the reinforcement particles form an alloy with metallurgical bonding [16].

The addition of micron-scale reinforcement particles such as Al_2O_3 or SiC a particulate into aluminum alloy matrix to form reinforced MMC has been developed for more than thirty years. After particulate reinforcement, the mechanical properties of metal matrix alloy are improved effectively so that

MMC has been applied to components requiring higher strength and light weight. The most common way of adding Al₂O₃ or Sic reinforcement particles is smelting. The particles are added into a liquid-phase material during the smelting process and are further stirred during the solidification process. Other than this process, there is hardly further technical information regarding adding particles into aluminum alloy for producing MMC [16]. In this present research reinforced particulates were added at weld interface by providing provision between two metal pieces to be weld. In this investigation, the effects of adding reinforced particulates at weld interface by studying mechanical properties of weld and microstructures.

2. Experimental Procedure

The material used for butt joints were 8mm thickness magnesium alloy AZ91 plate. The plates were machined to required dimensions of 100 mm X 75 mm X 8 mm. The plates were machined to get the desired geometry which was considered in figure1 and 2 to fill the reinforced particles and to provide interlocking between two pieces to be weld. Before welding the plates were cleaned chemically by ethanol to remove surface contaminations. Commercially available Al₂O₃ powder and Sic with sizes 99.9% pure was used. Separately The Al_2O_3 powder and SiC powder was filled into a groove of dimensions 3 mm (width) 3 mm (depth) 100 mm length machined on the plate of 8-mm thickness before the FSW was carried out. Reinforced particles such as silicon carbide and aluminium oxide were filled where the provision was provided to fill the reinforced particulates. H13 tool steel was used for welding AZ91 magnesium alloy having the shoulder diameter of 36mm. The tool had a pin height of 7.6 mm and a 12 mm pin diameter and taper profile. The vertical milling machine of HMT FM-2 and capacity of 10 H.P, 3000 R.P.M has been used to perform the welding process. The work pieces clamped to the fixture and the tool is placed in the tool holder by using collect of 25mm diameter. The initial welding has been done on the work pieces of Magnesium alloy AZ91 and Sic reinforced particulates at rotational speed of 1400 R.P.M and feed of 25mm/min and Second Welding has been done on the work pieces of Magnesium alloy AZ91 and Al₂O₃ at rotational speed of 1400 R.P.M and feed of 25mm/min. Temperatures were measured at different weld zones at different timings and at different spaces along the length of weld surface by using Infrared Thermometer of accuracy plus or minus 20C and with response time 500 ms.

After welding, the specimens were prepared by using wire EDM to test the mechanical properties such

Journal of Manufacturing Engineering, September 2015, Vol. 10, Issue. 3, pp 130-135

as Ultimate tensile strength, yield strength, impact strength and hardness at different weld zones.

2.1 Input data

Material	Magnesium Alloy AZ91
Thickness	8 mm
Length	100 mm each
Width	75 mm each
Rotational Speed	1400 R.P.M
Feed	25 mm/min
Reinforced Particulates:	Silicon Carbide (SiC) Aluminum Oxide (Al ₂ O ₃)
Experiment-1	Magnesium Alloy AZ91+ Silicon Carbide (SiC)
Experiment-2	Magnesium Alloy AZ91+ Aluminum Oxide (Al ₂ O ₃)

2.2 Friction stir welding tool



Fig.2 Friction Stir Welded tool

1-Tool Shank 2- Tool Shoulder 3- Tool Pin





Table 1. Chemical Composition of Base Meta	tal AZ91
--	----------

Element	Al	Zn	Mn	Cu	Si	Fe	Ni	Mg
Wt(%)	9.14	0.86	0.30	0.09	0.13	0.01	0.01	Rem.

Table 2. Mechanical Properties of Base Metal Mg alloy AZ91

Mg Allooy AZ91 Properties	Mg Allooy UTS AZ91 (MPA) Properties	YS (MPA)	% Elongation	HV	
ropentes	195	98	5.08	85	



Fig.5 FSW Joint of AZ91 with Sic



Fig.6 FSW Joint of AZ91 with Al_2O_3



Fig.7 Tensile specimen of FSW AZ91 with SiC Reinforced



Fig.8 Tensile specimen of FSW AZ91 with $Al_2O_3\ Reinforced$

www.smenec.org

3. Results and Discussions

The following results were obtained after conducting the Mechanical tests on friction stir welded joint of magnesium alloy AZ91 with additional SiC reinforced particulates at weld interface.

3.1 Output Data of Experiment-1

Ultimate Tensile strength	183.3 MPa
Yield Strength	146.64 MPa
Percentage of Elongation	3.81%
Final Gauge Length	51.907 mm
Load at Yield	14 KN
Load at Break	17.6 kN
Load at Peak	17.6 kN
Elongation at Yield	10.98 mm
Elongation at peak	13.58 mm

The Ultimate Tensile strength, Yield strength, and percentage of elongation of base metal AZ91 is 195 Mpa, 98 Mpa and 5.08% respectively. When the Magnesium alloy AZ91 was welded by Friction stir welding at 1400 R.P.M Rotational speed and 25 mm/min feed and adding additional Reinforcement particulates such as Silicon Carbide (Sic) at weld zone by 22.5% volume, The Mechanical properties were obtained as, Ultimate Tensile strength 183.3 Mpa, Yield Strength 136.260 Mpa, Percentage of Elongation 3.81%. By observing above results, the Ultimate tensile strength and Percentage of Elongation of Welded joint was decreased 6% and 25% respectively than base metal, but yield strength of welded joint was increased than base metal because due to adding of reinforced particulates such as Sic at weld portion. These Sic particles were dislocated in base metal hence failure of Specimen occurs at low strain and high stress because Silicon carbide was composed of tetrahedral of carbon and silicon atoms with strong bonds in the crystal lattice. This produces a very hard and strong material. Due to adding Sic particulates, it withstands more loads before plastic deformation. Hence the stress strain diagram shows a steeper curve with rapid formation of successive yield points due to quick diffusion and dislocations effects. Due to adding Sic particulates, hardness and impact strength of welded specimen was increased than base metal and increases brittleness than base metal.

The following results were obtained when Al_2O_3 Powder was used as additional reinforced particulates at weld interface.

3.2 Output Data of Experiment-2 174.6 MPa Ultimate Tensile strength Yield Strength 136.26 MPa Percentage of Elongation 4.02% Final Gauge Length 52.01 mm Load at Yield 13.08 kN Load at Break 14.99 kN Load at Peak 16.77 kN Elongation at Yield 24.65 mm Elongation at peak 27.27 mm

When, the Aluminum Oxide (Al₂O₃) Powder was used as additional Reinforcement particulates at weld zone by 22.5 % volume. The Mechanical properties were recorded as, Ultimate Tensile strength 174.689 Mpa, Yield Strength 146.64 Mpa, Percentage of Elongation 4.02 %. By observing above results, the Ultimate tensile strength and Percentage of Elongation of Welded joint was decreased by 10.4% and 20.8% respectively than base metal, but yield strength of welded joint was increased than base metal because due to adding of reinforced particulates such as Al₂O₃ at weld portion. These Al₂O₃ particles were dislocated in base metal hence failure of Specimen occurs at low strain and high stress. Aluminium oxide was from family of ceramics which provide enhanced mechanical properties. Due to adding Al₂O₃ particulates, it withstands more loads before plastic deformation. Hence the stress strain diagram shows a steeper curve with rapid formation of successive yield points due to quick diffusion and dislocations effects. Due to adding Al2O3Particulates, hardness and impact strength of welded specimen was increased than base metal and increases brittleness than base metal.



Graph. 1 Effect of Reinforced particulates on UTS





Graph. 2 Effect of Reinforced particulates on Yield Strength



Graph. 3 Effect of Reinforced particulates on % Of Elongation

Experimental results of friction stir welded joint of AZ91 with silicon carbide reinforced particles were compared with results of FSW join of AZ91 with Aluminium oxide reinforced particles, the weld joint with Sic reinforced particles obtained more Mechanical properties such as Ultimate tensile strength, Yield strength and hardness over weld joint with Al₂O₃ reinforced particles because Sic particles having yield strength was 10,000Mpa more harder than Al₂O₃ which yield strength was 5000 Mpa. But Percentage of elongation was reduced in FSW joint of AZ91 with Sic reinforced particles over weld joint with Al₂O₃ reinforced particles. This was due to more brittle nature of Sic over Al₂O₃ reinforced particles. So the FSW joint which was made with Sic Reinforced particulates were more brittle over FSW joint which was made with Al₂O₃ reinforced particles.

Due to adding of reinforced particulate at weld zone the hardness of weld was improved and it was varied from 90 HV to 110 HV in the stir zone and it was varied from 85-90 in the Heat affected zone.





Fig.9 Micro structure of Base metal AZ91 (10X)



Graph. 4 Phases of Base Metal AZ91



Fig.10 Microstructure at Stir Zone (10X)

www.smenec.org

Journal of Manufacturing Engineering, September 2015, Vol. 10, Issue. 3, pp 130-135



Fig.11 Microstructure at TMA Zone (10X)

Table 4. Grain Size Analysis

GrainSize analysis :Results Summary Fields measured 1

Analysed Area Standard used	.2376(sq mm) ASTM E 112	
ASTM Grain size#	8.5	
Intercepts	331	
Mean Int.length(um)	17.00558	
Std dev.	1.42	
95% CI		
%RA	124	

Magnesium alloy AZ91 consist of Two Phases i.e Alpha and Delta Phases and its percentages are 34.57and 65.43 respectively. It was observed that the grain size was refined and reformed in the stir Zone and TMAZ compared to base metal. Reinforced Particles such as Sic and Al₂O₃ were mixed and combined perfectly in the weld zone with base metal.

4. Conclusion

Mechanical Properties of friction stir welded joint of Magnesium alloy AZ91 was enhanced due to adding reinforced particulates such as Silicon carbide and Aluminium oxide at weld portion. By adding Reinforced particulates at weld portion, yield strength was increased than base metal. Effect of Sic reinforced particulates were more on the improvement of mechanical properties than Aluminium oxide. However adding of reinforced particulates can be change to enhance mechanical properties according to required applications and required mechanical properties.

References

- 1. Patent US7905383B1, (2011) "Manufacturing Method of Metal Matrix Composite using Friction stir welding", March15.
- Chang C I Du X H and Huang J C (2008), "Producing Nanograined micro structure in Mg-Al-Zn alloy by Two step friction stir processing", Science Direct, Script Materialia, Vol. 59, 356-359.
- 3. Chang C I Lee C J Huang J C (2004), "Relationship between grain size and Zener - Holloman parameter during friction stir processing in AZ31 Mg alloys", Scr. Mater.Vol. 51, 509–514.
- Chang C I Du X H Huang J C (2007), "Achieving ultrafine grain size in Mg-Al-Zn alloy by friction stir processing", Scr. Mater. Vol. 57, 209–212.
- Hsieh P J Lee C J Huang J C (2006), "Mg based Nano composites Fabricated by Friction Stir Processing", Scripta Materialia, Vol. 54, 1415-1420.
- Morisada Y Fujii H Nagaoka T Fukusumi M (2006), "MWCNTs/AZ31 surface composites fabricated by friction stir processing", Material Science Engineering-A., Vol. 419, 344– 348.
- Lee W B Lee C Y Kim M K Yoon J I Kim Y J Yoen Y M Jung S B (2006) "Microstructure and wear property of friction stir welded AZ91 Mg/SiC particle reinforced composite", Composite Science Technology, Vol. 66, 1513–1520.
- Suhuddin U F H R Mironov S Sato Y S Kokawa H Lee C W (2009), "Grain structure evolution during friction-stir welding of AZ31 magnesium alloy", ActaMater, Vol. 57, 5406–5418.
- 9. Lee S Lee S H and D H Kim (1998), "Metal. Mater", Tran. 29A, 1221–1235.
- 10. Munitz A Cotler C A Stern and Kohn G (2001), "Material science engineering", Vol. (A) 302, 68–73.
- 11. Lockyer S A and Russell M J (2001) "Proceedings of Third International Symposium on Friction Stir Welding", ed. by Treadgill P (The Welding Institute).
- Nakata S Inoki Nagano Y Hashimoto T Jorgan S and Ushio M (2001), J. of Jpn. Inst. of Light Met. Vol. 51, 528–533.
- Lee W B Yeon Y M Shae K Kim Kim Y J and S B (2002), "Jung: Magnesium Technology", ed. by Kaplan H I, (TMS (The Mineral, Metal and Materials Society)), 309–312.

www.smenec.org